

Ecole Centrale de Nantes

Project

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SIMUS

Goal

The objective is to implement the basic tools of **Matlab/Simulink** in order to simulate a state system described by nonlinear equations, and its associated control.

1 Control and differentiation

We consider the following system

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= x_3 \\ \dot{x}_3 &= -x_1 \cdot x_2 + x_3^2 + u\end{aligned}\tag{1}$$

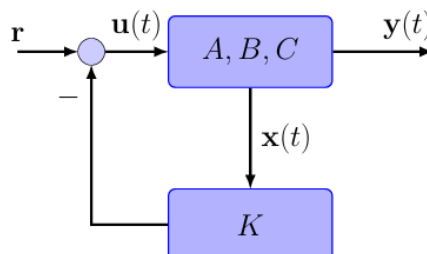
x_1 , x_2 , and x_3 being the state variables and u being the control input. The control is nonlinear in nature and defined by

$$u = x_1 \cdot x_2 - x_3^2 + v,\tag{2}$$

the term v being to be defined.

1. Show that the control u makes it possible to the system (1) be **linear**.

Then propose a control law v allowing x_1 to follow a sinusoidal trajectory with angular frequency 1 rad/s and amplitude 2. This control v will be based on linear state feedback (for tuning, use **acker** – multiple pole at -2).



2. Simulate the system (initial condition $[x_1(0) \ x_2(0) \ x_3(0)]^T = [0 \ 0.9 \ 0.1]^T$) and the control using Matlab functions, and choosing a **fixed-step** integration algorithm. Compare the simulation results with **Euler** and **Runge Kutta**, for increasingly larger sampling periods. **First, we assume that x_1, x_2 , and x_3 are measured.** Plot the state variables on one figure (use subplot) and the control input u on another figure.

3. We now use the Runge Kutta integration algorithm with $\tau = 0.1 \text{ ms}$. Suppose now that only the variable x_1 is measured, with variables x_2 and x_3 being estimated using two differentiators filtered by a first-order system

$$\frac{s}{1 + \tau_e s}$$

To evaluate the performance of this filter, first simulate the **filtered differentiators** in “open loop” (that is, the derivative estimates are not fed into the control law). Analyze the quality of the estimation as a function of the value of τ_e . Plot on the same figure x_2 and its estimate on one hand, and x_3 and its estimate on the other hand. Comment.

By setting $\tau_e = 1 \text{ ms}$, place the filtered estimates in the control loop, and plot x_1 and u .

4. Another technique for evaluating unmeasured variables is the use of an observer. From the system (1) to which we apply the control (2) (which yields a linear system), compute a **Luenberger**-type observer (multiple pole at -2). Using a *Matlab Function* block, integrate the observer into the simulator. Remember to initialize the observer with initial values different from those of the system ($[0, 1.1, 0.2]^T$). First test the observer not embedded in the control loop (plot the estimation errors), then in a second step, test the observer in the control loop. Verify that the estimation errors for all the state variables and the tracking error for x_1 converge to 0.

2 Dynamic control

We consider the nonlinear system

$$\begin{aligned}\dot{x}_1 &= \cos(x_3)u_1 \\ \dot{x}_2 &= \sin(x_3)u_1 \\ \dot{x}_3 &= u_2\end{aligned}\tag{3}$$

This system describes the dynamic behavior of a mobile robot in a plane, with x_1 and x_2 being the Cartesian coordinates. The objective is to control the two variables x_1 and x_2 . To achieve this, a nonlinear dynamic control is implemented and defined by

$$\begin{bmatrix} \dot{u}_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} \cos(x_3) & -\sin(x_3)u_1 \\ \sin(x_3) & \cos(x_3)u_1 \end{bmatrix}^{-1} \cdot \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}\tag{4}$$

Compute the two inputs v_1 and v_2 given that they aim to stabilize the following two subsystems

$$\begin{aligned}\ddot{x}_1 &= v_1 = -k_{11}\dot{x}_1 - k_{10}x_1 \\ \ddot{x}_2 &= v_2 = -k_{21}\dot{x}_2 - k_{20}x_2\end{aligned}\tag{5}$$

Set up a simulator to stabilize the system at the origin. Plot the system trajectory in the plane (x_1, x_2) , as well as the control inputs u_1 and u_2 .

3 Observer–Controller Duality

1. Consider the linear state–space system

$$\dot{x}(t) = Ax(t) + Bu(t), \quad y(t) = Cx(t).$$

1. Show that if the control law is chosen as

$$u(t) = -Kx(t) + r(t),$$

then the closed-loop dynamics of the system are governed by the matrix

$$A - BK.$$

2. Show that if we design a Luenberger observer of the form

$$\dot{\hat{x}}(t) = A\hat{x}(t) + Bu(t) + L(y(t) - C\hat{x}(t)),$$

then the estimation error dynamics are governed by the matrix

$$A - LC.$$

3. Explain briefly the role of the eigenvalues of $A - BK$ and $A - LC$.

4 Classical PI/PID Control

5. Consider the following system

$$G(s) = \frac{1}{s(s+1)}.$$

1. Manually design the gains of a PI/PID controller for this.
2. Use MATLAB's `pidTuner` to design a PID controller for $G(s)$, and compare the closed-loop performance with the manually designed controller. (Hint: you may use the syntax `pidTuner(G, 'PID')` to launch the interactive tuning tool.)
3. Plot and compare the step responses of both controllers using MATLAB. Comment on the differences in terms of overshoot, settling time, and steady-state error. (Hint: use `step(sys)` and `stepinfo(sys)` to analyze responses.)

5 Comparison of Control Methods

7. Consider a linear system in state-space form via feedback linearization used in q1.

$$\dot{x}(t) = Ax(t) + Bu(t), \quad y(t) = Cx(t).$$

Design three different controllers for this system:

- (a) A PID controller using `pidTuner`. (Hint: `pidTuner(G, 'PID')`)
- (b) A full-state feedback controller with pole placement, using the syntax

$$K = \text{acker}(A, B, \text{poles}) \quad \text{or} \quad K = \text{place}(A, B, \text{poles}).$$

- (c) An optimal controller using LQR, with the syntax

$$K = \text{lqr}(A, B, Q, R),$$

where Q and R are user-chosen weighting matrices.

Simulate and compare the closed-loop responses of the three approaches under the same initial conditions.

Comment on the advantages and limitations of each method.